

Citation:

Miles-Shenton, D (2018) Small Scale Forensic Thermal Imaging Study. Technical Report. Knauf Insulation.

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Document Version: Monograph (Accepted Version)

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Taylor Wimpey – Thermal Imaging Project

- Site: Kingsbrook Place Elmstree, Bury St Edmunds IP30 9HA
- Visit Date: 15th November 2017
- Plot(s): 8 & 9
- House Type: PA48 Shelford Full-fill Masonry, 2-Storey, 4-Bed Detached

REI STO 31: OF FIX BA 0 KITCHEN 2426 G 96 S BETW INDICATES RED 2 4 ۲ LOUNGE ⊕ BED 1 CHONER CHONER TRAY W5-12000F NOTES: 1. THE 2. THE AL RADIATOR SIZES ARE INDICATIVE ONLY. TALS OF GROUND FLOOR PLAN FIRST FLOOR PLAN REFER TO ENGINEER

Floor Plans: Plot 8 as below, Plot 9 handed version

Environmental Conditions:

Internal Temperature	22 °C	External Temperature	11.3 °C
Internal RH	57 %	External RH	84%
Wind Speed	0.0 ms ⁻¹	Wind Direction	n/a

Cloudy with some breaks in the clouds, overnight light rain but dry for preceding 3 hours.

Pressure Test Results Plot 9:

Depressurisation Only		Pressurisation	n Only	Mean			
m³/(h.m²)@50Pa	ach ⁻¹	r ²	m³/(h.m²)@50Pa	ach ⁻¹	m³/(h.m²)@50Pa	ach ⁻¹	
4.53	4.11	1.000	4.65	4.22	1.000	4.59	4.17



Observations:

The thermal images below are shown on varying temperature scales to highlight what was being observed, please take into account these different image spans when directly comparing images. The minimum span used is 5° so as not to over-exaggerate any thermal anomalies observed.

Thermal images under depressurisation were captured at an average pressure of -50.4 Pa.

External - Under natural conditions



Plots 8 & 9 are both SW facing and had been heated overnight. Plot 9 was surveyed first, by the time Plot 8 was surveyed there had been some light drizzle and breaks in the cloud allowing direct sunlight onto the roof.

Plot 8 External - Under natural conditions



There had been recent direct solar and drizzle prior to the external thermal survey for this property, affecting apparent surface temperatures.

9.0

Even reducing the thermal image span to 2.5° to intensify any surface temperature differences little extra can be observed besides warmer areas of walls where radiators are positioned internally:



The heat loss observed in the previous survey of this house type at the ground floor perimeter (Pipers Green, 08-Nov-2017) was not apparent on this site.



Plot 9 External - Under natural conditions









Plot 9 Lounge – Under natural conditions



Again, the external wall appeared marginally cooler at the bottom than was expected from just the natural temperature stratification in the room and the fact that the top part of the wall reflected the warm ceiling and the bottom part reflected the colder floor. The bay roof again showed minor cooler spots along the lines of the external wall above. There was also some noticeable cold air infiltration at the bay window without any induced negative pressure.



Flot 9 Lounge – Onder depressunsation



There appear to be some spots on the external wall where air is being drawn into the void behind the plasterboard directly from the external wall cavity, most probably due to gaps in the mortar in the inner leaf blockwork. This air from the cavity appears to have cooled the void behind the plasterboard



enough to reduce the temperature differential between areas of dry lining directly over and away from the adhesive dabs. The line of the external wall is more

distinct on the bay ceiling, as is air infiltration around the window and through/around the closed trickle vent.



Plot 8 Dining / Kitchen – Under natural conditions



Some additional thermal bridging around the patio doors was observed, in comparison to the kitchen window, where the patio doors were positioned further out into the external wall than the window, but nothing substantial. The external walls appeared to show a slightly decreased temperature gradient to those in the lounge.





Plot 9 Dining / Kitchen – Under depressurisation



Cold air infiltration was detected around some electrical service penetrations into the void behind the dry lining, including the outside light by the patio doors, and at the floor/ceiling junction by the boxedin SVP.

The patio doors appeared to allow a greater amount of air movement between the doors, between the doors and side lights and through/around the trickle vent.



Plot 8 Ground Floor WC – Under natural conditions



Plot 9 Ground Floor WC – Under depressurisation









The internal wall adjacent to the boxed-in services in the hall for the electric box and consumer unit appears even more distinct, possible due to air infiltration into this void under depressurisation; with a clear stratification along the study/hall partition from the external wall to where the hall radiator pipework remains visible. The gas meter box also remain welldefined, without air infiltration spreading out from it, indicating that the cooler patch here is due to it being less well insulated than the surrounding area rather than cold air entering through inner leaf wall penetrations.







Plot 9 Hall – Under depressurisation



Under depressurisation it appears that colder air is being drawn into the boxed-in service void, as differing wall temperatures can be seen below the consumer unit.





Plot 9 En-Suite – Under natural conditions





Cooler air is detected drawn in from the loft around recessed ceiling lights, into the internal partition walls, into the void behind the plasterboard on the external walls, into the bowed-in SVP riser and around some of the beading of the glazing panels.

Plot 8 Bedroom 1 – Under natural conditions



As in the En-suite there are some issues at the eaves but not as pronounced. The thermal gradient from floor to ceiling observed downstairs on the external walls is not present on the first floor where the floor and ceiling appear to be

Plot 9 Bedroom 1 – Under natural conditions



As observed in plot 8. There also appears to be additional cooler patches in the ceiling where the trussed rafter angled junctions prevent the loft insulation from being laid as effectively.

Plot 9 Bedroom 1 – Under depressurisation



Under depressurisation colder air can be seen being drawn down the dry lining voids on the external wall through gaps in the adhesive ribbons.

Cold air in the loft can also be seen tracking the cabling for the central ceiling light, emerging at the rose fitting.

There is some stratification between joists of the intermediate floor which was not observed from beneath.



Plot 8 Bedroom 4 – Under natural conditions









appear cooler than the window frame, and if condensation forms in the bathroom it will form on the coldest surfaces first, so may cause future issues.

20.5



Plot 9 Bathroom – Under natural conditions



As in plot 8, the coldest surface appears to be at the eaves junction.

Plot 9 Bathroom – Under depressurisation



As in the En-suite, cooler air is drawn in from the loft in many places.

The boxed-in service void to the right of the window was warmer than the external wall under natural conditions, under depressurisation it is now markedly cooler. Air was also detected in the void behind the toilet and basin, emerging around the soil pipe penetration.



Plot 8 Bedroom 3 – Under natural conditions





-	26.5 °C	
-		
	21.5	

Plot 9 Bedroom 3 – Under depressurisation





Plot 8 Bedroom 2 – Under natural conditions



Plot 9 Bedroom 2 – Under natural conditions











With cooler air being drawn in from the loft space the thermal images appeared quite different from those captured under natural conditions; with air movement around the loft hatch, other ceiling penetrations and partition wall junctions all becoming evident.





9.5	

Pressure Test Spreadsheet:

							DEPRESSURISATION					
		VERSIT	ŕ		Leed Insti	ls Sust tute	ainabil	ity	7.3 7.2 7.1			
MINNEAPOLIS BLOWER DOOR DATA INPUT AND CALCULATION							6.9		_			
date:	15/11/2017		Version 16d		19 June 2017				σ 68			
test house address:	Plot 9 - Kings	sbrook Place, Elm	swell, Suffolk, IF	30 9HA					5 67			
company:	Knauf Insula	tion - Taylor Wimp	ey						66-			
house type:	Shelford		,						65			
tester:	DMS								0.5			
test reference number:			Blower Door &	Gauge Used		Model 3 with	n DG700		6.4			
outdoor temp (°C)	11.3	°C	Note: ENSURE	THAT FLOW S	ETTINGS ARE IN m3/h	- When usin	g the DG70) gauge	6.3 +			
indoor temp (°C)	22	°C	run baseline pi	ressure adjustri	nent for minimum 60s v	vith fan switc	hed on but r	not	2.0		3.0 Ln ∆	P 4.0 5.0
outdoor humidity (%rh)	84.5	%RH	rotating									
indoor humidity (%rh)	57.2	%RH								1	PRESSURIS	ATION
outdoor barometric pressure	1013.1	mbar or hPa	Calculated Out	door Air Density	(L	1.24	kg/m ³	7.4 -			
Indoor barometric pressure	1013	mbar or hPa	Calculated Inde	oor Air Density			1.19	kg/m ³	7.2			
temperature corr. tact. depress.	0.964	WARNING!	Name Inc. it at	descri	ption of main constructi	on details:			1.3			/
temperature corr. tact. press.	1.038	Extreme test	ivew build, mas	sonry, blown full	-iiii, detached				7.2 -			1
baseline pressure diff (Pa) (+/-)	0	Pa							7.1 -			n 🖌
house width:	8.15	m	1						70-			
house depth:	8270	m	1						σ			F
house height:	4.92	m							5 ^{6.9}			
floor area:	129.05	m²							6.8			
volume:	317.47	m³							6.7 -			
envelope area including floor:	287.92	m²							6.6			
Pressure Difference for ELA	10	Pa							0.0			
RESULTS:		-							6.5 -			
Q50 Mean Flow at 50Pa =	1322.60	m³/h							6.4			
Mean Air Leakage at 50Pa =	4.17	h''							2.0		3.0 Ln.∆	P 4.0 5.0
Mean Air Permeability at 50 Pa =	4.59	m/h or m°h/m ²									=	-
Equivalent Leakage Area =	0.055	m ² at	10	Pa								Depressurisation
DEPRESSURISATION	RING -	MEASURED FAN	MEASURED	ADJUSTED	FLOW RANGE OK	Adjusted	Ln delta	Ln Q	Q50 Calculated	Permeability	Air Leakage	
	O,A,B,C,D,E	PRESSURE (Pa)	FLOW (m ^{-/} h)	FLOW (m %h)	FOR SELECTED	Pressure (Do)	P		Flow at 50Pa	Depressurisation	Depressurisation	1400.0
	0 1 2 3 for	Wax SUFa			KING?	(Fd)			(m²/n)	Only (m ⁻ /(n.m ⁻))	Only (n ')	1200.0
	DuctBB											1000.0
Approx 65 Pa	b	51.5	1366	1314.5	OK	51.5	3.942	7.181	1305.25	4.53	4.11	800.0
Approx 57 Pa	b	44.9	1257	1209.6	OK	44.9	3.804	7.098	r²	1.000		600.0
Approx 49 Pa	b	39.4	1157	1113.4	OK	39.4	3.674	7.015	Cerry	115.540	m³/h.Pa <i>n</i>	400.0
Approx 41 Pa	b	32	1017	978.6	OK	32	3.466	6.886	n	0.617		200.0
Approx 33 Pa	b	26.3	902	868.0	OK	26.3	3.270	6.766				0.0
Approx 25 Pa	b	19.7	757	728.4	OK	19.7	2.981	6.591	C _L (corrected)	116.838	m ³ /h Pa <i>n</i>	0 25 50 75 100
Approx 20 Pa	b	14.6	627	603.3	OK	14.6	2.681	6.402				ΔP
PRESSURISATION	RING -	MEASURED FAN	MEASURED	ADJUSTED	FLOW RANGE OK	Adjusted	Ln delta	Ln Q	Q50 Calculated	Permeability	Air Leakage	Pressurisation
	O,A,B,C,D,E	PRESSURE (Pa)	FLOW (m ³ /h)	FLOW (m ³ /h)	FOR SELECTED	Pressure	Р		Flow at 50Pa	Pressurisation	Pressurisation	1600.0
	for BD3	Max. 90 Pa			RING?	(Pa)			(m ³ /h)	Only (m ³ /(h.m ²))	Only (h ⁻¹)	1400.0
	0,1,2,3 for											1200.0
Annual CE De	DuctBB	50.5	4007	4454.0	01/	50.5	4.007	7.004	4000.00	4.05	4.00	1000.0
Approx 65 Pa	D	56.5	1397	1451.8	OK	56.5	4.034	7.281	1339.96	4.65	4.22	860.0
Approx 57 Pa	D	49.4	1285	1335.4	OK	49.4	3.900	7.197	r²	1.000		600.0
Approx 49 Pa	b	42	1163	1208.6	OK	42	3.738	7.097	Cerry	121.063	m³/h.Pa <i>n</i>	400.0
Approx 41 Pa	b	34	1018	1057.9	OK	34	3.526	6.964	n	0.615		200.0
Approx 33 Pa	b	28.4	914	949.8	OK	28.4	3.346	6.856				0 25 50 75 100
Approx 25 Pa	b	21	756	785.6	OK	21	3.045	6.666	C _L (corrected)	120.631	m³/h.Pa <i>n</i>	ΔΡ
Approx 20 Pa	b	15.8	639	664.0	OK	15.8	2.760	6.498				