



LEEDS
BECKETT
UNIVERSITY

Citation:

Wiesheu, M and Rutešić, L and Shukhobodskiy, AA and Pogarskaia, T and Zaitcev, A and Colantuono, G (2021) RED WoLF hybrid storage system: Adaptation of algorithm and analysis of performance in residential dwellings. *Renewable Energy*, 179. pp. 1036-1048. ISSN 0960-1481
DOI: <https://doi.org/10.1016/j.renene.2021.07.032>

Link to Leeds Beckett Repository record:

<https://eprints.leedsbeckett.ac.uk/id/eprint/7843/>

Document Version:

Article (Accepted Version)

Creative Commons: Attribution-Noncommercial-No Derivative Works 4.0

The aim of the Leeds Beckett Repository is to provide open access to our research, as required by funder policies and permitted by publishers and copyright law.

The Leeds Beckett repository holds a wide range of publications, each of which has been checked for copyright and the relevant embargo period has been applied by the Research Services team.

We operate on a standard take-down policy. If you are the author or publisher of an output and you would like it removed from the repository, please [contact us](#) and we will investigate on a case-by-case basis.

Each thesis in the repository has been cleared where necessary by the author for third party copyright. If you would like a thesis to be removed from the repository or believe there is an issue with copyright, please contact us on openaccess@leedsbeckett.ac.uk and we will investigate on a case-by-case basis.

1 RED WoLF Hybrid Storage System: Adaptation of
2 Algorithm and Analysis of Performance in Residential
3 Dwellings

4 Michael Wiesheu¹, Luka Rutešić², Alexander Alexandrovich Shukhobodskiy^{3*},
5 Tatiana Pogarskaia^{4**}, Aleksandr Zaitcev³, Giuseppe Colantuono³

6 ¹ *Technical University of Darmstadt, Darmstadt, Germany*

7 ² *University of Novi Sad, Novi Sad, Serbia*

8 ³ *Leeds Beckett University, Leeds, UK, LS1 3HE*

9 ⁴ *Peter the Great St.Petersburg Polytechnic University, St.Petersburg, Russia*

10 **Abstract**

11 The manuscript proposes the innovative energy storage technology which will
12 allow reducing the load from the grid during peak time consumption, as a result,
13 less CO2 will be generated by electrical grid or renewable energy such as wind
14 energy will not be wasted but rather stored in each household. We do not
15 manage the household consumption, but we store the energy whenever it is
16 “greenest“ and can be used in the future and at the same time avoid the usage
17 of the grid during the peak time, thus there is no effect on the dweller lifestyle.
18 Although the technologies used in the article are well known and are ready
19 to use, such a unique combination was never proposed before. We combine
20 photovoltaic arrays, storage heaters and batteries. The inclusion of storage
21 heaters allows us not to use the battery to heat the dwelling and consequently
22 dramatically reduce the battery size needed for the storage. The article also
23 shows the success in avoiding peak times of such combination during numerical
24 simulation test of the control algorithm. These results become exceptionally
25 interesting since this algorithm will be later tested on various pilot sites across
26 North Europe and thus innovate the energy sector.

27 *Keywords:* Hybrid Energy Storage, Battery, CO2 emissions, AI, Photovoltaic

28 **1. Introduction**

29 Global warming is a significant challenge for the environment and human
30 civilisation. The paramount influence in hastening the such an unfortunate sce-

*Lead Contact, a.shukhobodskiy@leedsbeckett.ac.uk

**Corresponding Contact, pogarskaya.t@gmail.com

CCS	Carbon Capture and Sequestration
DHW	Domestic Hot Water
EU	European Union
GHG	Green House Gases
HSS	Hybrid Storage System
NWE	North West Europe
PV	Photovoltaic
RED WoLF	Rethink Electricity Distribution Without Load Following
SHs	Storage heaters
The Grid	Electric Grid
The UK	The United Kingdom of Great Britain and Northern Ireland

List of Acronyms

31 nario is greenhouse gases (GHG). CO₂ is one of such gases that are emitted
 32 from fossil fuel power stations. Furthermore, association of electric grid (The
 33 Grid) CO₂ emission level to produced kWh of energy is uneven throughout a
 34 day. In more details for each kWh produced by the electric grid the amount of
 35 CO₂ in grams emitted by the grid is given by the CO₂ intensity index. That
 36 phenomena is illustrated in figure 1. The reason behind uneven energy gener-
 37 ation throughout a day is mainly due to uneven energy consumption, which
 38 triggers on demand fossil fuel power plants to satisfy the momentary consump-
 39 tion. This is due to renewable power plants corresponding to solar, hydro and
 40 wind energy as well as nuclear power stations are very limited in their flexibil-
 41 ity to modulate energy generation. In order to fix the problem and reduce the
 42 dependency on "dirty" on demand power plants, the energy storage must be
 43 implemented either on the side of power generator or on the side of the final
 44 consumer. Furthermore, the residential sector in Europe produces 30% of total
 45 GHG emission. Therefore, tackling this sector is of utmost importance for
 46 achieving sustainability.

47 Significant amount of research was produced in order to solve such an issue
 48 throughout recent years. Potential strategies of a battery storage were exces-
 49 sively studied in [1]. The effects of changing climate on daytime peak hours of
 50 power demand are discussed in [2]. In the work [3] it was shown that battery
 51 storage technologies can provide significant peaking capacity contributions on
 52 example of the case of 18 regions in the United States. Optimisation of the dis-
 53 charging/charging process of electrical storage is investigated as a cost-effective
 54 way to benefits through load shifting in [4]. Microgrids control management for
 55 batteries was discussed in [5]. The article [6] presents the latest achievements in
 56 thermal storage for the time period between 2009 and 2017. In the [7] the au-
 57 thors suggested that financial benefit might be achieved by smartly combining
 58 heat pump and thermal storage. Furthermore, another scenario was studied in
 59 [8], where both heat pump and domestic hot water cylinder (DHW cylinder) are
 60 joined together. Later that idea was developed by adding electrochemical stor-
 61 age further and analysed theoretically in [9] and experimentally in [10]. Such a
 62 configuration could lead to reduction of an operational cost. Intriguingly, such
 63 systems could lead to significant increase of the construction costs. In opposition
 64 to the aforementioned articles, this work was performed with the aim of both

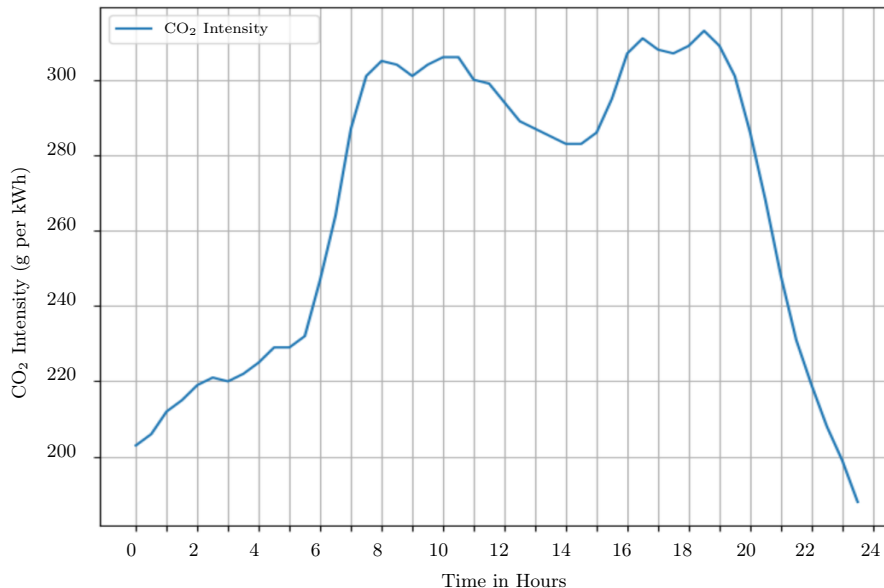


Figure 1: Exemplary data of the CO₂ Grid intensity level over a day.

65 optimising the financial expenditure and reducing the environmental impact. In
 66 the [11] the authors provided excessive review of strategies in order to improve
 67 PV generated energy self-consumption. To reduce peak demand, an approach
 68 based on storing energy during off-peak periods or during periods of solar energy
 69 availability and then using it during peak periods was proposed in [12]. Peak
 70 demand shifting was discussed with the aid of batteries in [13]. [14] achieves
 71 similar results by cleverly managing the equipment within the dwelling. In the
 72 work [15] the authors coupled the Grid, with a battery and thermal storage
 73 other than Storage Heaters (SHs) to minimise the intake from the Grid. The
 74 smart combination of SHs, a Battery, a PV array and DHW cylinder allows
 75 to achieve similar results in the absence of pipework associated with central
 76 heating and heat pumps. In [16] and [17] the authors produced comprehensive
 77 reviews of pathways to CO₂ reduction. In [18] the authors suggested that the
 78 demand management could be added on top of storage systems to improve the
 79 latter performance. Furthermore, in [19] the authors reviewed the advances in
 80 AI control for renewable energy systems.

81 Wholesale energy has a potential to reach negative price [20]. Moreover, on
 82 demand energy in case of time of use tariff has the similar ability [21]. Unfortu-
 83 nately wind energy generation [22, 23, 24] could produce a mismatch between
 84 power generation and the consumption. A similar phenomena could be also ob-
 85 served in the case of the solar energy called a *duck curve* [25, 26]. As a result, it
 86 is paramount to develop a system which would be able to improve the usability
 87 of renewable system through smart storage. Different types of energy storage
 88 systems were investigated in recent years. Depending on their storage meth-

ods the systems can be divided into 4 groups with mechanic, electrochemical, electromagnetic and phase change energy storage modes [27, 28, 29, 30]. One such system is the RED WoLF Hybrid Storage System (HSS) first mentioned in [31]. The system consists of smart coupling of the SHs, a DHW Cylinder, a battery and a PV array. There are both physical and financial reasons for such a choice of components. First of all, these components remove all associated costs with plumbing work related to central heating systems, allowing the additional budget to be used for the installation of the system components. Secondly, the presence of SHs allows to reduce the capacity of a battery in order to achieve peak shifting. SHs are not only significantly cheaper than a battery, with high end state-of-the-art models costing at least ≈ 10 times less, but also to convert 100% of the Grid energy into heat. Finally, the multiple countries start to phase out domestic gas usage from heating applications. For example the Netherlands has a plan to phase out gas heating by 2050 [32] and the UK by 2025 [33]. This leads to high level of demand for fully electrical dwellings as proposed by the RED WoLF.

Interestingly, SHs are not well represented throughout the world. Despite that SHs significantly improved their performance throughout multiple years and could produce significant impact in the era of renewable and sustainable energy. In some countries where such heating devices are common are the UK, Republic of Ireland, France and Australia. In the UK, Republic of Ireland and Australia the rise of the storage heaters is related to deindustrialisation, where excess energy produced by inflexible coal power plants was needed to be stored in order to sustain the Grid operation. Such a solution was successful, however was later phased out by gas central heating due to coal plants decommissioning. In France such a solution is related to the overabundance of nuclear energy generation, which could be modulated, however not on the scale of fossil fuels power plants.

The RED WoLF HSS is planned to be installed throughout 100 dwellings in 6 pilot sites within North-West Europe (NWE) under regional development project [34]. These pilot sites are located within 3 different countries, namely France, the Republic of Ireland and the UK. These countries have different wiring and the Grid standards, which add additional level of complexity for system designs throughout the testing stage. Nevertheless, such differences are providing the unique opportunity to test the design and control throughout with multiple possible setups. The pilot sites would provide the unique data that would be later compared and enhanced with the numerical simulation presented in current work.

1.1. Novelty

The basic RED WoLF system [31] is an important step towards a more sustainable future. Achieving carbon emission reduction secures a more lively environment, and changes the direction our society is heading in. The core purpose of this work is to improve the performance of progressive threshold approach and adapt the controlling logic for international applications, in order to minimise the CO₂ output.

134 Instead of trying to reduce the operation cost or energy consumption, the
 135 RED WoLF system achieves significant savings in CO₂ by shifting the energy
 136 peak demand to times of low CO₂ Grid intensities. As decarbonisation of the
 137 electricity system is an immediate goal of several countries, replacing the wet
 138 heating system and using the Grid for heating purposes are important steps to
 139 fulfil CO₂ reduction targets and attain independence from fossil fuels.

140 In this manuscript we expand the idea of progressive threshold approach
 141 described in [31] and employed for systems equipped with battery only in [35].
 142 Two new algorithm strategies recursive strategy and normalisation strategies are
 143 proposed in order to boost the performance of the algorithm. The limitations
 144 and benefits of these approaches are tested in a numerical simulation performed
 145 in two different countries France and the UK, for systems with various battery
 146 capacities and PV arrays.

147 2. RED WoLF hybrid storage system

148 In order to reduce the dependencies from the Electric Grid, the system must
 149 be able to satisfy the demand for heating, hot water and electric energy for
 150 household appliances. Therefore the RED WoLF components consist of stor-
 151 age heaters (SHs) for space heating, a DHW cylinder for hot water storage and
 152 a battery for electricity supply. For efficiency reasons, a PV array is also in-
 153 cluded as a component in the RED WoLF system. The power distribution is
 154 coordinated by the In-house Programmable Logic Controller (PLC), which uses
 155 predictions for the PV output and the home demand for heat, hot water and
 156 electricity. Further predictions are made for the CO₂-intensity, updated and
 157 adjusted to the real data every hour. In this way, the electrical demand that
 158 cannot be covered by the PV array itself is adjusted to the time interval when
 159 the CO₂-intensity of the Grid is the lowest (except for the appliances which are
 160 powered on demand). In the case of energy excess, the PV array will also supply
 161 the Grid after fully loading the system components.

162 After determining the estimated energy demand and production, the RED
 163 WoLF system handles the energy distribution of the dwelling. The schematic
 164 energy flow is shown in Figure 2.

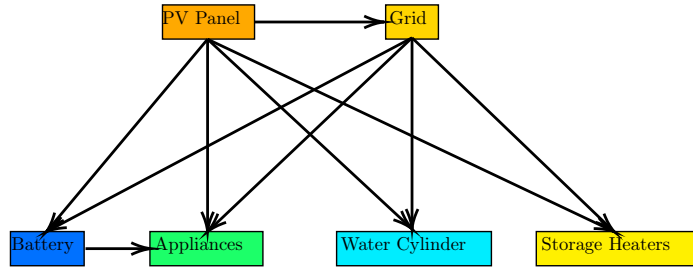


Figure 2: Schematic representation of the energy flow in a dwelling using the RED WoLF System (based on representation presented in: [31])

165 *2.1. The basic RED WoLF Algorithm*

166 In this subsection we will carefully explain how does the base RED WoLF
 167 algorithm function. We ought to explain the decision making, and showcase the
 168 procedure. Firstly, a list of all variables that our system uses is provided in
 169 Table 1.

Notice that some of the parameters are predefined locally, and are depending on the house equipment ($H_{\text{IMax}}, \tilde{H}_{\text{IMax}}, B_{\text{IMax}}, C_{\text{IMax}}$ and B_{Max}). Others, for example H_{Setup} and C_{Setup} , are adjustable by the dwellers or automatically set up for a fixed period of time. Necessary inputs for a legitimate simulation are the 24h PV generation forecast (P_{PV}), household consumption forecast (P_{P2A}) and the 24h CO₂ intensity from the Grid forecast (Q). The base system will operate in the time span of 24h, which we will later optimise to work for multiple days. In what follows we write Grid intake, for power intake from the grid to the dwelling. Heat, battery and cylinder demand are defined in the following way:

$$\tilde{H}_D = \tilde{H}_{\text{IMax}} \cdot \Theta(\tilde{H}_{\text{Setup}} - \tilde{H}_{\text{level}}), \quad (1)$$

$$B_D = B_{\text{IMax}} \cdot \Theta(B_{\text{Setup}} - B_{\text{level}}), \quad (2)$$

$$C_D = C_{\text{IMax}} \cdot \Theta(C_{\text{Setup}} - C_{\text{level}}), \quad (3)$$

170 where $\Theta(x) = \begin{cases} 1 & \text{if } x > 0, \\ 0 & \text{if } x \leq 0. \end{cases}$ and $\Theta(x)$ is dimensionless Heaviside step
 171 function.

172 This means that unless the storage fulfils the daily required energy, the
 173 power demand for the storage is the maximum rate of intake, otherwise, it is
 174 zero. Next, we will make an introduction to the integral balance of the system:
 175

$$\begin{aligned} \mathbb{I} &= \frac{1}{60} \int_{\hat{t}}^{\mathbb{T}} (P_{P2A}(t) - P_{PV}(t)) dt + C_{\text{Setup}} - C_{\text{Level}} \\ &\quad + \tilde{H}_{\text{Setup}} - \tilde{H}_{\text{Level}}. \end{aligned} \quad (4)$$

Variable t represents time, \hat{t} is the current time and \mathbb{T} is the time up to which the prediction is made (in minutes). We should also note that division by 60 in the right-hand side of Equation (4) is needed to transform kWmin to kWh. This integral defines the difference between the total energy demand and the energy generated by the PV array. Hence, \mathbb{I} is an energy quantity in kWh and describes the accumulation of energy in the considered period of time. In the case when $\mathbb{I} \leq 0$, the amount of generated energy is larger than what is needed for consumption. However, if $\mathbb{I} > 0$, the predicted generated energy is lower than the required energy. Consequently, we can modify the time we supply the house with the Grid energy based on forecasts. In other words, when PV generation forecast is high, the Grid is used a lot less. The rate of power intake

$B_{I\text{Max}}$	Maximum rate of battery intake in kW
B_{Max}	Maximum battery capacity in kWh
$C_{I\text{Max}}$	Maximum rate of Cylinder intake in kW
$H_{I\text{Max}}$	Maximum rate of house intake from Grid in kW
$\tilde{H}_{I\text{Max}}$	Maximum rate of heat intake in kW
B_D	Battery demand in kW
B_{level}	Battery level in kWh
B_{setup}	Energy required to be stored in a battery in 24h in kWh
C_D	Cylinder demand in kW
C_{level}	Cylinder level in kWh
C_{Setup}	The energy required by user to be obtained in 24h in kWh
E	Excess of power generation in kW
\tilde{H}_D	Heat demand in kW
\tilde{H}_{level}	Heat level in kWh
\tilde{H}_{Setup}	The energy needed for SHs to obtain in 24 h in kWh
\mathbb{I}	The integral balance of the system
P_{P2A}	Predicted power to appliance in kW
P_{PV}	Predicted power from PV in kW
\hat{t}	Current time in min
T_{PV}	Actual power from PV in kW
T_{P2B}	Actual power to battery in kW
T_{PFB}	Actual power from battery in kW
T_{P2H}	Actual power for heating in kW
T_{P2C}	Actual power to Cylinder in kW
T_{PFG}	Actual power from Grid in kW
T_{P2G}	Actual power to Grid in kW
T_{P2A}	Actual power to Appliances in kW
\mathbb{T}	Duration of forecast in min
T_{int}	Time of the Grid energy intake in min
Q	CO ₂ intensity level prediction in gCO ₂ /kWh
Q_{sort}	Sorted in monotonically increasing order array of CO ₂ intensity level predictions in gCO ₂ /kWh
δ	CO ₂ intensity threshold in gCO ₂ /kWh
Θ	The Heaviside step function.

Table 1: Predefined parameters and variables

is defined as:

$$\tilde{\omega} = \min(\omega, H_{I\text{Max}}), \quad (5)$$

where,

$$\omega = \int_{\hat{t}}^{\mathbb{T}} P_{P2A}(t) dt / \mathbb{T} + \tilde{H}_{\text{IMax}} + C_{\text{IMax}} + B_{\text{IMax}}. \quad (6)$$

176 where $\min(x_1, x_2, \dots, x_n)$ is the a function which chooses the minimum values
 177 between $x_1 \wedge x_2 \wedge \dots \wedge x_n \forall x_1, x_2, \dots, x_n \in \mathbb{R}$ (\wedge is logical and, \forall is for all, \in
 178 means belongs to the set), with dimensions being preserved. The power intake is
 179 the sum of the storage demands and the average appliances intake and therefore
 180 a power quantity.

181 Time for which we are allowed to intake power is the following:

$$\mathbb{T}_{\text{int}} = 60 \left[\max \left(\frac{\mathbb{I}}{\tilde{\omega}}, \frac{C_{\text{Setup}} - C_{\text{Level}}(\hat{t})}{C_{\text{IMax}}}, \frac{H_{\text{Setup}} - H_{\text{Level}}(\hat{t})}{H_{\text{IMax}}} \right) \right], \quad (7)$$

182 where $\max(x_1, x_2, \dots, x_n)$ is the a function which chooses the maximum values
 183 between $x_1 \wedge x_2 \wedge \dots \wedge x_n \forall x_1, x_2, \dots, x_n \in \mathbb{R}$ and multiplication by 60 is used
 184 to make dimensions of T_{int} minutes.

185 Q is the array of predicted values of CO_2 intensity level for the next 24
 186 hours period with one minute step resolution. Rearranging Q in monotonically
 187 increasing order grants us a monotonically increasing array Q_{sort} . By doing so,
 188 it is possible to define the CO_2 threshold, above which we are not allowed to
 189 take energy from the Grid to charge the components:

$$\delta = Q_{\text{sort}}(\mathbb{T}_{\text{int}}) \text{ for } \mathbb{I} > 0, \text{ or } \delta = 0 \text{ for } \mathbb{I} \leq 0. \quad (8)$$

190 In other words, if $\delta \leq Q(t)$, we won't supply from the Grid. In that case, if
 191 $T_{P2A} \geq T_{PV}$ (the power from PV does not cover the demand), power is drawn
 192 from the battery to supply the appliances. However if the battery is insufficient,
 193 we rely on the Grid. Thus:

$$T_{PFG} = (T_{P2A} - T_{PV}) \cdot \Theta \left(\frac{T_{P2A}}{60} - \frac{T_{PV}}{60} - B_{\text{level}} \right), \quad (9)$$

$$T_{PFB} = (T_{P2A} - T_{PV}) \cdot \Theta \left(\frac{T_{P2A}}{60} - \frac{T_{PV}}{60} - B_{\text{level}} \right). \quad (10)$$

194 Here we divide by 60 within the Heaviside step function in order to transform
 195 power in kW to energy in kWh used in one minute. On the other hand, if
 196 $T_{P2A} \leq T_{PV}$, there is excess PV power: $E = T_{PV} - T_{P2A}$. This excess can be
 197 spent on different ways, based on its quantity.

198 **Case 1.** $E < C_D$.

In this case we transfer all of the surplus power to the water cylinder. Thus:

$$T_{P2C} = E \cdot \Theta(C_{\text{Setup}} - C_{\text{level}}). \quad (11)$$

199 **Case 2.** $E \geq C_D \wedge E < C_D + \tilde{H}_D$.
 Here,

$$T_{P2C} = C_D, \quad (12)$$

$$T_{P2H} = (E - C_D) \cdot \Theta(\tilde{H}_{\text{Setup}} - \tilde{H}_{\text{level}}). \quad (13)$$

200 This would mean that the water cylinder is our priority, since we supply it
 201 first.

202 **Case 3.** $E \geq C_D + \tilde{H}_D \wedge E < C_D + \tilde{H}_D + B_D$.
 Therefore our algorithm is as follows:

$$T_{P2C} = C_D, \quad (14)$$

$$T_{P2H} = \tilde{H}_D, \quad (15)$$

$$T_{P2B} = \min((E - C_D - \tilde{H}_D), B_{\text{IMax}}) \cdot \Theta(B_{\text{Max}} - B_{\text{level}}). \quad (16)$$

203 This is done with the intention to charge the battery as much as possible.

204
 205 **Case 4.** $E \geq C_D + \tilde{H}_D + B_D$
 Finally:

$$T_{P2C} = C_D, \quad (17)$$

$$T_{P2H} = \tilde{H}_D, \quad (18)$$

$$T_{P2B} = B_D, \quad (19)$$

$$T_{P2G} = E - (C_D + B_D + \tilde{H}_D). \quad (20)$$

206 Here we export the excess power to the Grid, as we have sufficient energy.
 207 Now, lets assume that $Q < \delta$. The maximum power that can be directed into
 208 the house is

$$M_{HPV} = H_{\text{IMax}} + T_{PV}. \quad (21)$$

209 As the CO₂ level is below the threshold, we are allowed to use the Grid
 210 energy. Our equations now become:

$$T_{P2C} = \min(C_D, (M_{HPV} - T_{P2A}) \cdot \Theta(C_{\text{Setup}} - C_{\text{level}})), \quad (22)$$

$$T_{P2H} = \min(\tilde{H}_D, (M_{HPV} - T_{P2A} - T_{P2C}) \cdot \Theta(\tilde{H}_{\text{Setup}} - \tilde{H}_{\text{level}})), \quad (23)$$

$$T_{P2B} = \min(B_D, (M_{HPV} - T_{P2A} - T_{P2C} - T_{P2H}) \cdot \Theta(B_{Max} - B_{level})) \quad (24)$$

211 In the case of PV energy surplus, we are able to feed all the excess power
 212 into the Grid. We update the CO₂ intensity threshold only if the demand of
 213 SHs and the water cylinder is not satisfied as a result of it deviating from the
 214 starting predictions. This can be beneficial when the original predictions differ
 215 from the actual energy generation and consumption.

216 Below in Figure 3 is the plot of the CO₂ intensity along with the generated
 217 thresholds based on the power of the PV. We could notice how the threshold is
 218 getting higher, the weaker the PV is. That means, if the PV has more power,
 219 the system will supply from the Grid less, and rely more on the photo-voltaic
 220 array.

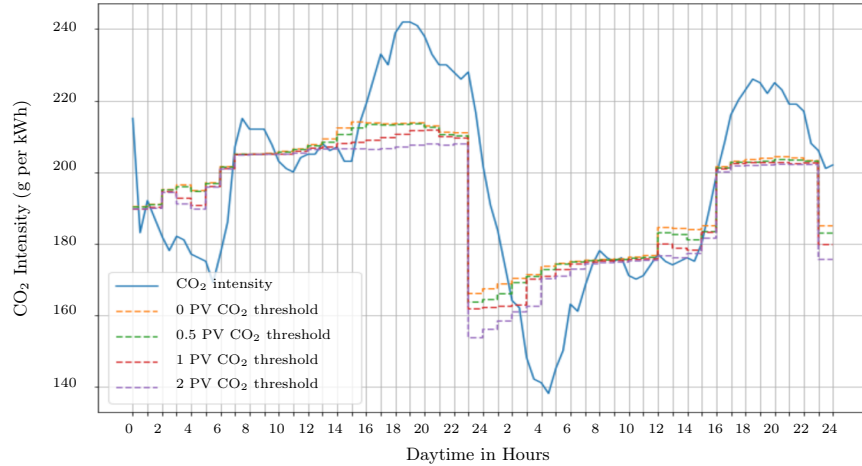


Figure 3: Different CO₂ thresholds based on the power of PV. 0, 0.5, 1, 2 correspond to the variation of the original PV array by multiplication on the mentioned values.

2.2. Progressive threshold approach - the normalised version

222 One major problem with the basic version of the RED WoLF algorithm is,
 223 that the introduction of a CO₂ threshold does not guarantee that space heating
 224 and hot water are always available. Since the CO₂ intensity is usually low in
 225 the morning and in the afternoon, the intervals, when the Grid is used, are set
 226 accordingly. With an especially low CO₂ intensity level in the afternoon, it can
 227 happen, that the storage is not loaded in the morning, despite the need for heat
 228 or hot water. Therefore it is not guaranteed that the energy levels of the SHs
 229 or the Hot Water Cylinder do not decrease to zero due to the consumption of
 230 heat or hot water. In the worst scenario, the CO₂ intensity minimum at the
 231 end of the day are always below those of the previous day and the new global

232 minimum is selected for loading the storage. This could result in unheated
 233 houses for numerous days, until the CO₂ intensity level rises again.

234 We are proposing two approaches to correct this problem. The first one
 235 is advance the calculation method for the CO₂ threshold. There are always
 236 two days compared by the algorithm, so we use the energy consumption and
 237 generation predictions for at least the next 25 hours. The hours before 12
 238 o'clock at night are considered the first day, the hours after the second day.
 239 This method consists of four steps, that are visualised in Figure 4:

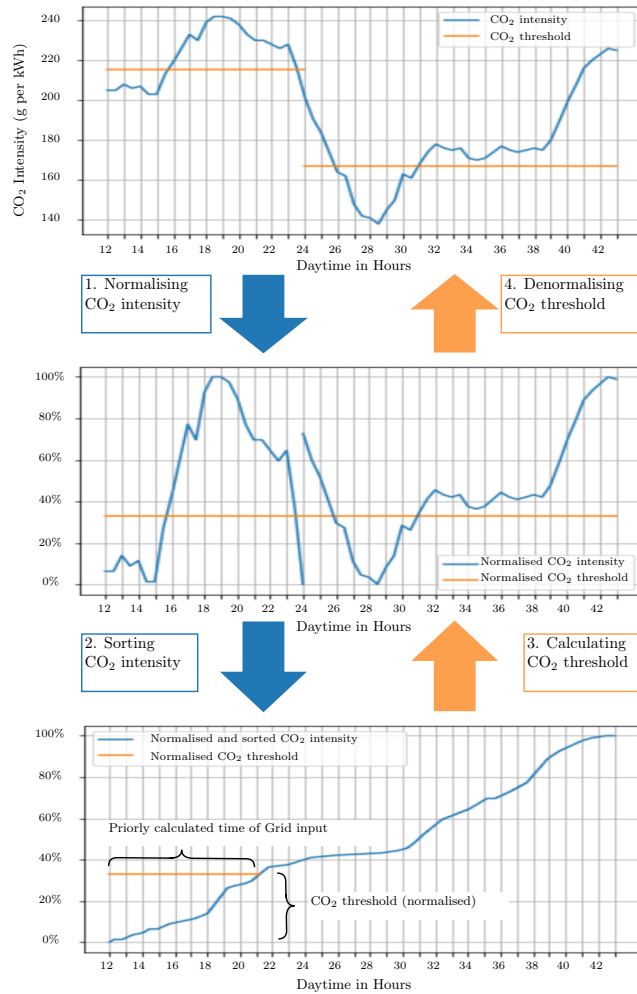


Figure 4: Process of calculating the CO₂ threshold by normalising two consecutive days and denormalising the CO₂ threshold.

240 **1. Normalising the CO₂ intensity:** By normalising the CO₂ intensity
 241 data for each day, local CO₂ intensity minimum, that occur on the current

242 day, are as equally important as global minimum on the next day. This
 243 avoids long time intervals without energy intake from the Grid.

- 244 2. **Sorting the CO₂ intensity:** This step is the same as calculating the
 245 CO₂ threshold for the basic algorithm. The only difference is that the
 246 normalised CO₂ intensities are used instead of the real ones.
- 247 3. **Calculating the normalised CO₂ threshold:** The normalised CO₂
 248 threshold is the value at the calculated time of Grid intake \mathbb{T}_{int} , as ex-
 249 plained in the previous subsection. The calculation for \mathbb{T}_{int} did not change.
- 250 4. **Denormalising the CO₂ threshold:** With the known maximum and
 251 minimum CO₂ intensity levels for each day, the normalised CO₂ threshold
 252 is being denormalised for the current and the next day, resulting in a
 253 different CO₂ thresholds for each day.

254 This normalisation technique creates scenarios that are much more stable
 255 compared to a calculation method with a single CO₂ threshold.

256 Nevertheless, while normalising the CO₂ intensity levels balances the usage
 257 of the Grid, it is still not guaranteed, that the heat or cylinder level falls to zero.
 258 Due to unforeseen circumstances, the energy consumption and generation will
 259 always differ from the predictions. So the second idea we introduce here is force
 260 charging. Heating and hot water should be always available, so if the energy
 261 level of the SH or the water cylinder decreases to zero, it will be forced charged
 262 one hour until the CO₂ threshold is updated again, no matter the CO₂ intensity.
 263 This limits the efficiency of the system for the rare case of exceptionally high
 264 energy demands, but at this point assuring energy supply is more important
 265 than saving CO₂.

266 *2.3. Progressive threshold approach - the recursive version*

267 The basic RED WoLF algorithm calculates the optimal time for Grid usage,
 268 but it is not verified, that the scenario is possible without empty storage reser-
 269 voirs. So another method to stabilise the algorithm, is to check, if the scenario
 270 works with simplified assumptions (evenly distribution of heat and hot water
 271 demand), and recalculate the simulation with less prediction time, if the heat
 272 or hot water level falls below zero. This is where the idea of ‘recursive’ comes
 273 from: If the scenario is not feasible, retry it with less prediction time, until it
 274 works. If the standard RED WoLF algorithm fails due to low CO₂ intensities
 275 in the future, the enhanced recursive algorithm successively removes the future
 276 predictions, which lead to infeasible results.

277 The recursive method also starts with 24 hours of prediction, as the standard
 278 algorithm does. If the feasibility check works, then the CO₂ threshold from
 279 the standard algorithm is used. If this is not the case, then one hour less of
 280 prediction will be used, so 23 hours in this case. This continues, until a CO₂
 281 threshold is found, that minimises the used CO₂ Grid intensities without the
 282 danger to run out of storage capacity or need to force charge. If there is no CO₂
 283 threshold found for one hour of prediction, the maximum CO₂ intensity of that
 284 interval is returned, such that the system is allowed to charge.

285 Figure 5 shows how the recursive system works. We can see that in the
 286 first iteration heat levels drop below zero. Therefore, we calculate the optimal
 287 threshold once again with one hour shorter predictions. At one point, when the
 288 threshold gets high enough, the heat levels stabilise, as we are allowed to use
 the grid more often.

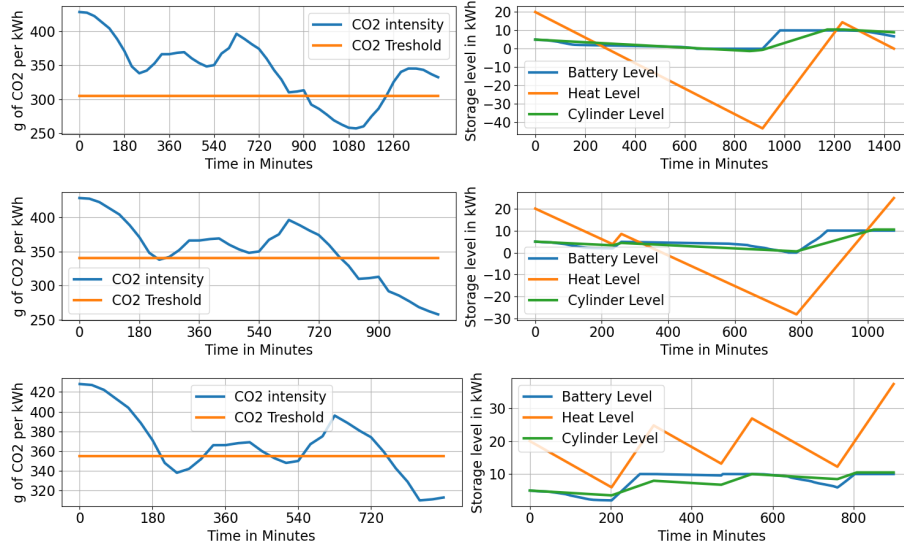


Figure 5: Three steps of the recursive enhancement for the REDWoLF algorithm. Panels on the left correspond to creation of optimal thresholds the avoids force charges. Panels on the right represents storage levels, with top two failing to achieve point in order to avoid force charging.

289 This method still needs the ability to force charge, as the predictions for
 290 heat, hot water and appliances consumption will differ from reality, but as the
 291 algorithm combines the ‘perfect’ threshold from the standard algorithm with a
 292 reality check to avoid force charging in times of high CO₂ intensities, the results
 293 are both very stable and effective. A drawback compared to the normalising
 294 method is that it is computationally more expensive because of the recursive
 295 iterations. But this should not be much of a problem in the real application,
 296 because the computations only need to be performed once every hour.
 297

298 2.4. Adapting the RED WoLF Algorithm for different environments

299 Further adapting energy distribution for storage may result in better system
 300 performance. Different countries have different housing infrastructures, thus our
 301 strategy may not be the most efficient one in some parts of the world. However,
 302 we are able to adapt the system, and make it work optimally in various regions.
 303 Namely, the maximum rate of house intake ($H_{I\text{Max}}$) deviates in European coun-
 304 tries, hence the energy spending priorities must change. For example, in the
 305 UK we know that: $H_{I\text{Max}} = 25kW$, while in Belgium it is usually much lower:
 306 $H_{I\text{Max}} = 9kW$.

307 We propose that for countries with relatively low maximum house intake the
 308 battery has to be charged first, whether we are above or below the threshold.
 309 When the CO₂ intensity is above the threshold and we have excess PV energy,
 310 we should examine whether that surplus is larger than the battery demand
 311 (instead of the cylinder demand, as we did before). After supplying the battery,
 312 the cylinder, SHs and the Grid are provided with the power respectively.

313 In the case when the intensity is below the threshold, the algorithm is as
 314 follows:

$$T_{P2B} = \min(B_D, (M_{HPV} - T_{P2A}) \cdot \Theta(B_{Max} - B_{level})), \quad (25)$$

$$T_{P2C} = \min(C_D, (M_{HPV} - T_{P2A} - T_{P2B}) \cdot \Theta(C_{Setup} - C_{level})), \quad (26)$$

$$T_{P2H} = \min(\tilde{H}_D, (M_{HPV} - T_{P2A} - T_{P2B} - T_{P2C}) \cdot \Theta(\tilde{H}_{Setup} - \tilde{H}_{level})) \quad (27)$$

315 The idea behind these changes is that the battery now charges the appli-
 316 cances most of the time, and it is used more often than in the previous version
 317 of the system. The savings are now higher when the PV panels are weak, as
 318 we are distributing energy efficiently with this improved algorithm (it would
 319 have been much lower with the old system). In Figure 6, we demonstrate how
 320 our algorithm functions for multiple days in the UK case. The storage levels,
 321 the CO₂ data and the power flow for the components are plotted. In order
 322 to simulate the performance of the system we take PV power generation and
 323 appliance consumption from [36] and [37], respectively. These data was previ-
 324 ously used in [38] and [31]. We should note that [37] data were detrended from
 325 seasonal effects, which may contribute to heating and normalised to 5 MWh
 326 annual consumption for electric appliance in the UK and France in accordance
 327 to [39].

328 The main area of application of the RED WoLF algorithm is the regions
 329 with climates, where the heating is necessary, but cooling is not present. Never-
 330 theless the initial algorithm could work in different circumstances as well. [35]
 331 concluded that the original RED WoLF algorithm, is stable even in presence of
 332 PV panel and battery only and could lead to savings in CO₂ emissions up to 37
 333 %. Furthermore, the system as it is has potential to accommodate cooling. The
 334 one of the possible solutions is to add the prediction of cooling consumption to
 335 the prediction appliance consumption in order to calculate CO₂ threshold. It is
 336 also possible to add new section to the algorithm responsible for cooling. The
 337 exact strategy would depend on the implemented cooling technology.

338 The RED WoLF system is designed to separate thermal storage and storage
 339 required for appliance consumption. This would allow to reduced the financial
 340 expenditure required for the system installation. The cost reduction is achieved
 341 by employing SHs instead of batteries for the space heating and domestic hot
 342 water. SHs with the same amount of energy capacity are significantly cheaper

343 than batteries. Low-tier SHs could cost as low as ≈ 200 GBP per 15 kWh. Mid-
 344 tier and high-tier have prices significantly higher and could cost from ≈ 500 GBP
 345 to ≈ 1000 GBP with ≈ 24 kWh capacity. Nevertheless, the price is significantly
 346 lower, than the one of the batteries where price for 1 kWh capacity is around
 347 1000 GBP. Furthermore, storage heaters are 100 % efficient and all the energy
 348 input is transformed directly to heat. As a result the price of an average system
 349 with 4 kW PV array, 5 SHs, 2 kWh battery and a water cylinder is around 7050
 350 GBP (installation cost included). Moreover, we should note that SHs could
 351 be connected to the power socket directly without any additional work. Thus,
 352 making them easy substitution for high capacity batteries, for space heating
 353 applications.

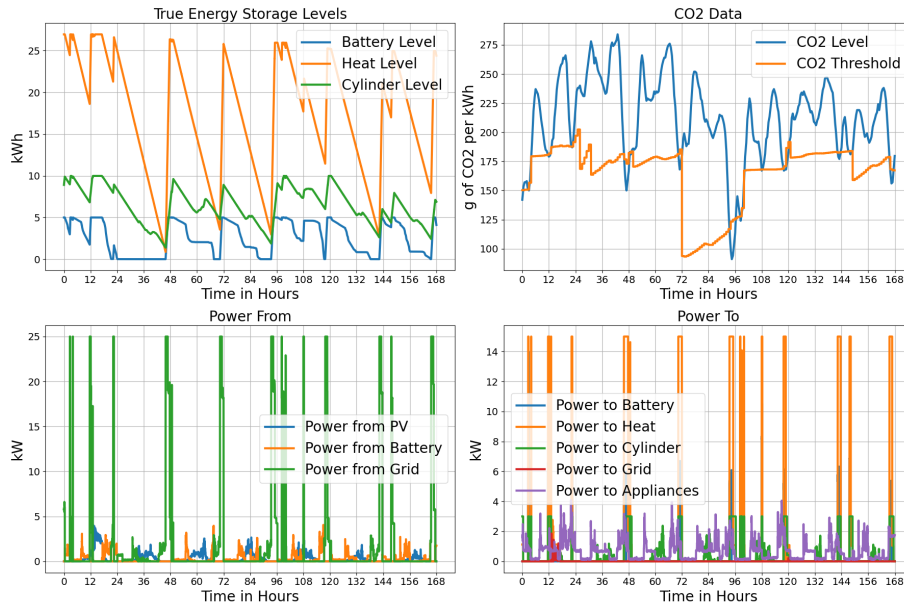


Figure 6: Power flow and CO₂ threshold for one week in spring in the UK. Recursive version is used for threshold calculation.

354 2.5. Application of the RED WoLF Algorithm using existing data as input

355 At this point, the progressive threshold approach implemented in the RED
 356 WoLF is ready for different countries and seasons. Additional scenarios with
 357 different PV array sizes will also be tested (half size, double size and no PV).
 358 To date, there is no detailed data for the daily consumption of hot water and
 359 space heating, for the systems composed of the RED WoLF elements, so some
 360 assumptions are necessary for the distribution of the yearly demand, which
 361 is known. So we assume that most of the space heating (75%) is needed in
 362 winter, there is no space heating in summer and the remaining heating is equally
 363 distributed to spring and autumn. The yearly need for heat in kWh for certain

364 countries is shown in table 2. With the aid of [40] and [41], the maximum rate
 365 of house intake from the grid is for different countries is considered, although
 366 the exact rate might vary for some specific energy providers and tariffs.

country	Yearly heat demand [kWh]	Max rate of house intake [kW]
Spain	4291	5.5
Italy	9595	15
UK	12037	25
Poland	12084	25
France	12305	12
Germany	13572	34
Ireland	15816	25
Belgium	16630	9

Table 2: Yearly energy demand per dwelling and maximum rate of house intake for specific countries.

367 3. Results

368 In the previous chapter we introduced two methods in order to improve
 369 the standard RED WoLF algorithm and create stable scenarios for multiple
 370 days. The two techniques proposed are Normalising of the CO₂ intensities and
 371 Recursive solving. Furthermore, we introduced the origin of main data used in
 372 the numerical experiment.

373 To determine the performance of each algorithm, different scenarios were
 374 simulated with each version using historical data from 2018 in the UK (figure
 375 7) and France. Table 3 lists the relative savings for different PV and battery
 376 sizes for the Standard, Normalise and Recursive version of the RED WoLF al-
 377 gorithm obtained with the aid of the numerical experiment. During this study
 378 it was assumed that the power input to all system components could vary from
 379 0 to maximum nominal power continuously. Moreover, the heat and hot water
 380 consumption is spread throughout the day evenly. The later assumption
 381 could underestimate the positive impact of the algorithm on CO₂ reduction due
 382 since in majority of standard dwellings the main consumption occurs in day and
 383 "peak" hours [42]. However, as such system has not being tried to be imple-
 384 mented before, these results could provide sufficiently good estimates of systems
 385 performance and guarantees safety before it could be tested in pilot sites that
 386 would be occupied with residents. Similarly to [31], we assume that power flow
 387 in each minute is different to the one predicted by adding white noise to histori-
 388 cal one. Such a process allows to present the system stability. That could differ
 389 to the planned pilot sites case, where all the predicted consumption and the
 390 grid CO₂ intensity index would be generated via machine learning techniques
 391 and would be unique for each single dwelling. The percentage savings refer to a

392 dwelling without storage reservoir but electric heating on demand that emits 4
 393 tons of CO₂ over the year. Moreover, the main assumptions are as follows. The
 394 hot water consumption is the same for both the France and the UK. The heating
 395 pattern is the same, however the overall heat consumption is normalised for the
 396 yearly demand provided by table 2, to take into account the difference between
 397 two countries. Furthermore, we assume the dwellings in both countries have the
 398 same size of the PV array and a battery capacity, which is then scaled in the
 399 numerical investigation. The appliance consumption is the same for both cases,
 400 and the prediction for appliance consumption is different for the same white
 401 noise. The PV generation and prediction for the UK and France are different,
 402 since the countries have different geographical locations.

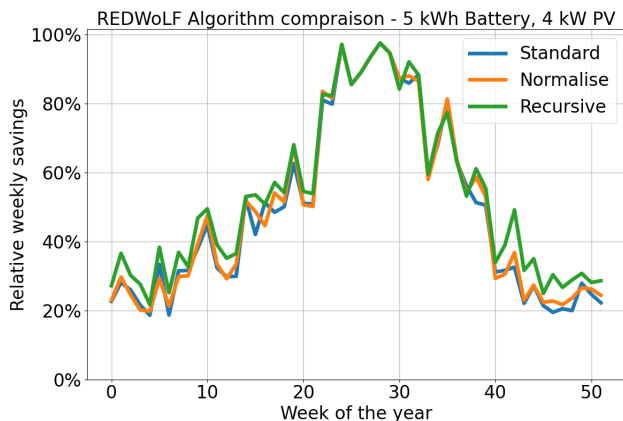


Figure 7: Simulated weekly relative savings of CO₂ of the REDWoLF System in the UK for the different types of algorithms with a 5 kWh battery and a 4 kW PV array.

403 The first discovery follows from figure 7. We can conclude the recursive
 404 version is very stable in operation and performs best for all scenarios. The
 405 normalisation of CO₂ intensities usually yields better results compared to the
 406 standard algorithm, but the improvement is much lower than expected. While
 407 normalisation is advantageous if force charging is avoided, the use of local min-
 408 ima seems to be a disadvantage when it is not needed.

409 Since the recursive algorithm clearly outperforms the other versions, it will
 410 be used in the following analyses. In figure 8 different battery sizes are used
 411 with a 4 kW PV array. Again the relative savings of CO₂ are compared to a
 412 dwelling that uses the Grid for heating and appliances on demand. The relative
 413 savings fluctuate for each week, depending on the CO₂ intensities, PV generation
 414 and electric demand, but the overall trend becomes clear: Low PV generation
 415 and high heat demand result in lower savings in winter months, whereas high
 416 PV generation and low heat demand result in high relative savings in summer
 417 months. The larger the battery size, the greater the savings, which is also to
 418 be expected. The difference in relative savings is most evident in the summer
 419 months, as the battery is charged only by PV.

Battery	0 kWh Battery			2.5 kWh Battery			5 kWh Battery			7.5 kWh Battery			10 kWh Battery		
Version*	S	N	R	S	N	R	S	N	R	S	N	R	S	N	R
0 kW PV	14.9	15.4	20.0	15.8	16.2	21.4	17.1	17.6	22.9	18.2	18.7	24.1	19.1	19.5	25.2
2 kW PV	24.5	24.7	29.4	25.5	25.7	30.9	26.7	27.1	32.3	27.7	28.0	33.4	28.5	28.8	34.2
4 kW PV	31.3	31.8	36.2	33.0	33.6	38.2	34.3	35.0	39.8	35.3	36.0	41.0	36.0	36.7	41.7
8 kW PV	40.5	40.4	44.6	42.7	42.8	47.2	44.4	44.7	49.1	45.4	45.7	50.3	46.1	46.4	51.0

Table 3: Relative percentage savings of CO₂ comparison for the UK depending on the PV and battery size

*, *S*, *N* and *R* stand for *standard*, *normalising* and *recursive REDWoLF* system respectively

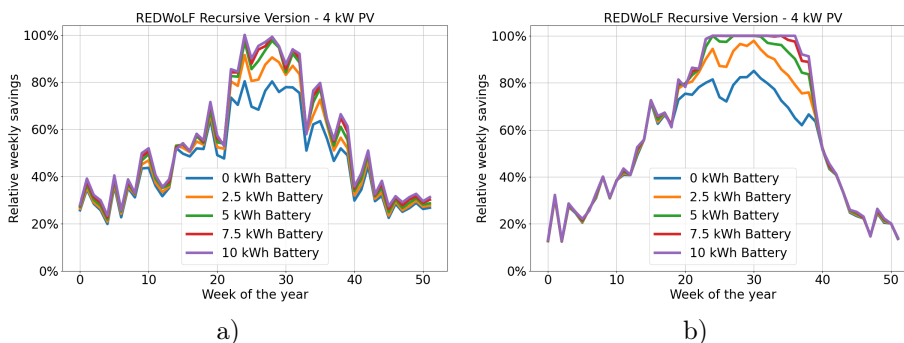
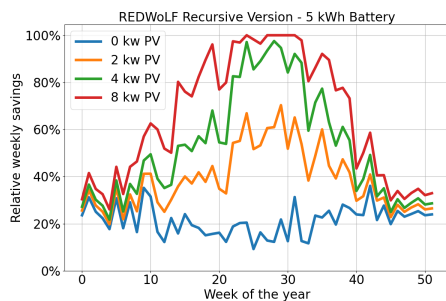


Figure 8: Simulated weekly relative savings of CO₂ of the RED WoLF System in the UK (a) and France (b) compared to a house with electric heating on demand. The standard 4 kW PV array is compared with varying battery sizes.

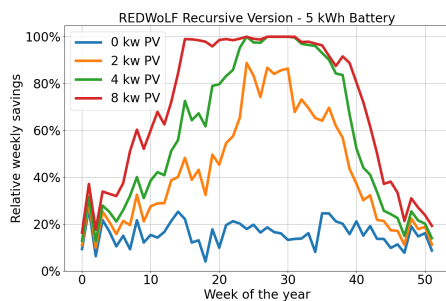
420 The same observation can be made comparing different PV array sizes. The
421 weekly savings are shown in figure 9a for a 5 kWh battery. Again the relative
422 savings fluctuate for each week primarily due to different CO₂ intensities and
423 PV generation. One major difference is that varying the PV size also significantly
424 changes the savings, much more compared to the battery size. This is
425 also expected as Solar provides carbon free electricity, whereas the battery re-
426 distributes the Grid usage. Having a large PV array even results in 100 percent
427 of savings in certain weeks in summer, making the dwelling independent from
428 the Grid.

429 As gas and oil heating is still common in different regions throughout the EU,
430 we eventually compare a RED WoLF-dwelling with different heating systems
431 (equipped with 5kWh Battery and 4kW PV). The absolute CO₂ emission for
432 each week is shown in figure 10. With 650 grams of CO₂ equivalents per kWh,
433 heating with oil results in more than 10.1 tons of CO₂ over the year. Heating
434 with gas is better than oil, but with 490 grams of CO₂ equivalents per kWh
435 and about 7.9 tons of CO₂ yearly still extremely bad, considering 4 and 2.4
436 tons of yearly CO₂ emissions for electric heating and the RED WoLF system.
437 Abstaining from oil and gas for heating purposes is necessary in order to meet
438 the CO₂ reduction goals.

439 It has become clear, that the RED WoLF system is able to reduce the CO₂



(a) UK



(b) France

Figure 9: Simulated weekly relative savings of CO₂ of the REDWoLF System in the UK (a) and France (b) compared to a house with electric heating on demand. The standard 5 kW PV array is compared with varying battery sizes.

440 emissions for a dwelling in the UK drastically. The RED WoLF system with
 441 a 4 kW PV array and a 5 kWh battery saves from about 40 % (compared to
 442 direct heating) to 69 % (compared to gas heating) and even 76 % (compared to
 443 oil heating).

444 As circumstances differ for every country, we also test the RED WoLF system
 445 for a different country: France. The data sets for CO₂ intensity, heating and
 446 PV generation are taken from [43]. The uniqueness of France is the low CO₂
 447 Grid intensities due to high use of nuclear energy. Table 4 provides the relative
 448 savings over a year for France. The results are similar to the UK, where the
 449 recursive RED WoLF algorithm performs best and Normalising is slightly better
 450 than the Standard version. The reference is again a house with electric heating
 451 on demand, but the CO₂ emissions for this dwelling in France are about 740
 452 kilograms.

453 The relative weekly savings for different battery sizes for France are shown
 454 in figure 8b. These values are higher compared to the UK mainly due to higher
 455 PV production in France. The overall trend is the same.

456 Emissions with the RED WoLF systems are drastically lowered, as Figure 10
 457 shows. Depending on the type of heating, the carbon footprint we leave varies

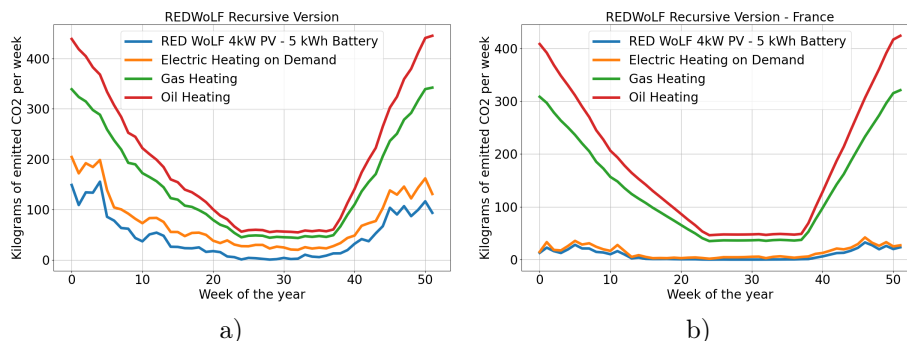


Figure 10: Simulated weekly absolute CO₂ emissions for different heating systems in the UK (a) and France (b)

Battery	0 kWh Battery			2.5 kWh Battery			5 kWh Battery			7.5 kWh Battery			10 kWh Battery		
	S	N	R	S	N	R	S	N	R	S	N	R	S	N	R
0 kW PV	11.5	10.8	13.3	12.1	11.5	14.1	12.8	12.1	14.9	13.4	12.5	15.5	13.9	12.7	16.0
2 kW PV	24.7	23.9	26.3	25.5	24.7	27.2	26.1	25.1	27.7	26.5	25.3	28.1	26.9	25.5	28.5
4 kW PV	32.6	31.9	34.3	34.2	33.4	35.9	35.1	34.2	36.8	35.6	34.5	37.3	35.9	34.7	37.6
8 kW PV	44.8	44.1	46.2	46.6	45.7	48.1	47.6	46.7	49.1	48.1	47.1	49.6	48.2	47.2	49.7

Table 4: Yearly relative percentage savings of CO₂ comparison for France depending on the PV and battery size

**, S, N and R stand for standard, normalising and recursive RED WoLF system respectively*

458 a lot. We can notice that using the RED WoLF, the carbon discharge is much
 459 lower compared to the traditional systems. Specifically, compared to the yearly
 460 emissions for direct heating on demand (740 kg CO₂), gas heating (7.1 tons
 461 CO₂) and oil heating (9.3 tons CO₂) the RED WoLF system (468 kg) with 4
 462 kW PV and 5 kWh battery saves about 37 %, 93 % and 95 % respectively. It is
 463 clear that heating with fossil fuels is so much worse, as the CO₂ Grid intensity
 464 is low in France.

465 The simulations performed are based on measured data for PV generation,
 466 real electricity and real CO₂ intensity thus although the results are estimates,
 467 they are close to the real life case. These assumptions are based on under-
 468 standing of possible operational capabilities of the equipment. SHs are able to
 469 store up to 80% of heat withing 3 day period. However, this heat is not lost
 470 as it makes the dwelling warmer. The operation time frame of the system is 24
 471 hours, that makes the SHs technology appropriate and not prone to large errors
 472 in the estimates. The same holds truth for the hot water cylinder. The water
 473 boiler insulation is sufficient to keep water hot within required time frame of the
 474 system operation. The heating requirements for both water and space heating
 475 during that period could outweigh the requirements in appliances consumption
 476 for up to 10 times. Furthermore, white noise was added to the consumption
 477 profiles, in order to guarantee that even in the wrong consumption prediction
 478 the system would operate. Thus, the results of numerical simulation, coincides

479 with expectation of the system performance. Therefore, they could be used as
480 a guidance for the system operation.

481 4. Conclusions

482 The ability to find the adequate threshold, which serves as an indicator to
483 change the energy supplier and store heat, is the key feature of the RED WoLF
484 algorithm. It is worth noticing that thermal demand is not to be satisfied with
485 the battery output, due to conversion losses and relatively large amount of en-
486 ergy required for heating. However, during simulation phase there was found
487 a limitation in original RED WoLF algorithm for cases with low power supply
488 from the grid. Thus we introduced additional logic for such cases. Moreover
489 on top of that two different techniques were developed in order to improve the
490 performance of progressing threshold approach. The first one includes normal-
491 isation techniques which on average slightly outperforms by $\approx 1\%$ the original
492 RED WoLF algorithm. The second techniques include recursive action, which
493 leads to more significant savings of $\approx 5\%$.

494 The performed numerical simulation are promising with the system equipped
495 with 5 kWh battery and 4 kW PV array the system could save 39.8% of CO₂ in
496 the UK and 36.8% of CO₂ in France. Furthermore, the total energy consumption
497 of the RED WoLF system produces by far less CO₂ than the one that would
498 only be spent on space heating by gas and oil systems. That statement holds to
499 be true even in the UK, where high penetration of fossil fuel plants is present.
500 Furthermore, there is a difference that is hard not to notice in the UK case
501 between systems equipped with the RED WoLF or not. In France there is even
502 greater margin between electric heated houses and ones equipped with gas or
503 oil. In terms of CO₂ the difference between the RED WoLF and conventional
504 electric house is not that great in absolute values. That could be explained
505 by high nuclear power plant penetration, which lowers the electrical grid CO₂
506 emissions. Thus for France the best recommendation is to adapt the progressive
507 threshold approach to time of use tariff signal. More intriguingly, for some
508 system configurations significant period of time corresponding to 100% CO₂
509 savings, making the system self sufficient both for France and the UK. Which
510 shows the ultimate potential of such system configuration.

511 The fact that the cost of electrical energy usually follows the CO₂ intensity
512 levels introduces an alternative motive for pursuing changes the RED WoLF
513 offers. Namely, the benefit of the system is therefore not only the reduction of
514 CO₂ emissions, but also the decrease of the heating cost, which accounts for
515 more than 10% of the household income in certain regions [44]. Nevertheless, a
516 more detailed study is needed to be done in order to estimate the potential of
517 the system in cost reduction. As the number of renewable energy providers sup-
518 plying the electrical grid increases, the system also stabilises the Grid. Overall,
519 it can be said that the system has numerous advantages and is in many ways
520 superior to traditional heating systems.

521 **Acknowledgemnt**

522 MW, LR, AS, AZ, GC are thankful to Interreg Northwest Europe for the
523 support received to conduct this research through grant number: NWE847.
524 MW, LR, AS, TP acknowledge support by the Academic Excellence Project
525 5-100 proposed by Peter the Great St.Petersburg Polytechnic University.

526 **References**

- 527 [1] M. Sufyan, N. A. Rahim, M. M. Aman, C. K. Tan, S. R. S. Raihan, Sizing
528 and applications of battery energy storage technologies in smart grid sys-
529 tem: A review, *Journal of Renewable and Sustainable Energy* 11 (1) (2019)
530 014105.
- 531 [2] H. Ullah, I. Kamal, A. Ali, N. Arshad, Investor focused place-
532 ment and sizing of photovoltaic grid-connected systems in pak-
533 istan, *Renewable Energy* 121 (2018) 460–473. doi:<https://doi.org/10.1016/j.renene.2017.12.048>.
534 URL <https://www.sciencedirect.com/science/article/pii/S0960148117312521>
535
536
- 537 [3] P. Denholm, J. Nunemaker, P. Gagnon, W. Cole, The potential for battery
538 energy storage to provide peaking capacity in the united states, *Renewable*
539 *Energy* 151 (2020) 1269–1277.
- 540 [4] X. Han, T. Ji, Z. Zhao, H. Zhang, Economic evaluation of batteries plan-
541 ning in energy storage power stations for load shifting, *Renewable Energy*
542 78 (2015) 643–647. doi:[https://doi.org/10.1016/j.renene.2015.01.](https://doi.org/10.1016/j.renene.2015.01.056)
543 056.
- 544 [5] A. K. Arani, G. B. Gharehpetian, M. Abedi, Review on energy storage
545 systems control methods in microgrids, *International Journal of Electrical*
546 *Power & Energy Systems* 107 (2019) 745 – 757. doi:[https://doi.org/](https://doi.org/10.1016/j.ijepes.2018.12.040)
547 10.1016/j.ijepes.2018.12.040.
- 548 [6] J. Yan, X. Yang, Thermal energy storage, *Applied Energy* 240 (2019) A1
549 – A6. doi:<https://doi.org/10.1016/j.apenergy.2018.03.001>.
550 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261918303179)
551 S0306261918303179
- 552 [7] B. Felten, C. Weber, The value(s) of flexible heat pumps – assessment
553 of technical and economic conditions, *Applied Energy* 228 (2018) 1292 –
554 1319. doi:<https://doi.org/10.1016/j.apenergy.2018.06.031>.
555 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261918309000)
556 S0306261918309000
- 557 [8] B. Baeten, F. Rogiers, L. Helsen, Reduction of heat pump induced peak
558 electricity use and required generation capacity through thermal energy

- 559 storage and demand response, *Applied Energy* 195 (2017) 184 – 195.
560 doi:<https://doi.org/10.1016/j.apenergy.2017.03.055>.
561 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261917302854)
562 [S0306261917302854](http://www.sciencedirect.com/science/article/pii/S0306261917302854)
- 563 [9] S. Kuboth, F. Heberle, A. König-Haagen, D. Brüggemann, Economic
564 model predictive control of combined thermal and electric residen-
565 tial building energy systems, *Applied Energy* 240 (2019) 372 – 385.
566 doi:<https://doi.org/10.1016/j.apenergy.2019.01.097>.
567 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261919300996)
568 [S0306261919300996](http://www.sciencedirect.com/science/article/pii/S0306261919300996)
- 569 [10] A. Baniasadi, D. Habibi, W. Al-Saedi, M. A. Masoum, C. K. Das,
570 N. Mousavi, Optimal sizing design and operation of electrical and ther-
571 mal energy storage systems in smart buildings, *Journal of Energy Storage*
572 28 (2020) 101186. doi:<https://doi.org/10.1016/j.est.2019.101186>.
- 573 [11] R. Luthander, J. Widén, D. Nilsson, J. Palm, Photovoltaic self-
574 consumption in buildings: A review, *Applied Energy* 142 (2015) 80 – 94.
575 doi:<https://doi.org/10.1016/j.apenergy.2014.12.028>.
576 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261914012859)
577 [S0306261914012859](http://www.sciencedirect.com/science/article/pii/S0306261914012859)
- 578 [12] J. Romanía, M. Beluskob, A. Alemub, L. F. Cabezaa, A. Graciac,
579 F. Brunob, Control concepts of a radiant wall working as thermal energy
580 storage for peak load shifting of a heat pump coupled to a pv array, *Re-
581 newable Energy* 118 (2018) 489–501.
- 582 [13] E. McKenna, M. McManus, S. Cooper, M. Thomson, Economic
583 and environmental impact of lead-acid batteries in grid-connected
584 domestic pv systems, *Applied Energy* 104 (2013) 239 – 249.
585 doi:<https://doi.org/10.1016/j.apenergy.2012.11.016>.
586 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261912008094)
587 [S0306261912008094](http://www.sciencedirect.com/science/article/pii/S0306261912008094)
- 588 [14] J. Widén, Improved photovoltaic self-consumption with appliance schedul-
589 ing in 200 single-family buildings, *Applied Energy* 126 (2014) 199 – 212.
590 doi:<https://doi.org/10.1016/j.apenergy.2014.04.008>.
591 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261914003419)
592 [S0306261914003419](http://www.sciencedirect.com/science/article/pii/S0306261914003419)
- 593 [15] F. Reda, Z. Fatima, Northern european nearly zero energy building
594 concepts for apartment buildings using integrated solar technolo-
595 gies and dynamic occupancy profile: Focus on finland and other
596 northern european countries, *Applied Energy* 237 (2019) 598 – 617.
597 doi:<https://doi.org/10.1016/j.apenergy.2019.01.029>.
598 URL [http://www.sciencedirect.com/science/article/pii/](http://www.sciencedirect.com/science/article/pii/S0306261919300297)
599 [S0306261919300297](http://www.sciencedirect.com/science/article/pii/S0306261919300297)

- 600 [16] M. Wagh, V. Kulkarni, Modeling and optimization of integration of renew-
601 able energy resources (rer) for minimum energy cost, minimum co2 emis-
602 sions and sustainable development, in recent years: A review, *Materials*
603 *Today: Proceedings* 5 (1, Part 1) (2018) 11 – 21, international Confer-
604 ence on Processing of Materials, Minerals and Energy (July 29th - 30th)
605 2016, Ongole, Andhra Pradesh, India. doi:[https://doi.org/10.1016/](https://doi.org/10.1016/j.matpr.2017.11.047)
606 [j.matpr.2017.11.047](https://doi.org/10.1016/j.matpr.2017.11.047).
- 607 [17] D. Grosspietsch, M. Saenger, B. Girod, Matching decentralized energy pro-
608 duction and local consumption: A review of renewable energy systems
609 with conversion and storage technologies, *WIREs Energy and Environment*
610 8 (4) (2019) e336. arXiv:[https://onlinelibrary.wiley.com/doi/pdf/](https://onlinelibrary.wiley.com/doi/pdf/10.1002/wene.336)
611 [10.1002/wene.336](https://onlinelibrary.wiley.com/doi/pdf/10.1002/wene.336), doi:10.1002/wene.336.
- 612 [18] M. Uddin, M. F. Romlie, M. F. Abdullah, S. A. Halim, A. H. A. Bakar,
613 T. C. Kwang, A review on peak load shaving strategies, *Renewable and*
614 *Sustainable Energy Reviews* 82 (2018) 3323 – 3332. doi:[https://doi.](https://doi.org/10.1016/j.rser.2017.10.056)
615 [org/10.1016/j.rser.2017.10.056](https://doi.org/10.1016/j.rser.2017.10.056).
- 616 [19] P. Boza, T. Evgeniou, Artificial intelligence to support the integration of
617 variable renewable energy sources to the power system, *Applied Energy*
618 290 (2021) 116754. doi:[https://doi.org/10.1016/j.apenergy.2021.](https://doi.org/10.1016/j.apenergy.2021.116754)
619 [116754](https://doi.org/10.1016/j.apenergy.2021.116754).
620 URL [https://www.sciencedirect.com/science/article/pii/](https://www.sciencedirect.com/science/article/pii/S0306261921002646)
621 [S0306261921002646](https://www.sciencedirect.com/science/article/pii/S0306261921002646)
- 622 [20] N. Ederer, The market value and impact of offshore wind on the electricity
623 spot market: Evidence from germany, *Applied Energy* 154 (2015) 805 –
624 814.
- 625 [21] Octopus Energy, Octopus energy agile (2020).
626 URL [octopus.energy](https://www.octopus.energy)
- 627 [22] N. Zhang, X. Lu, M. B. McElroy, C. P. Nielsen, X. Chen, Y. Deng, C. Kang,
628 Reducing curtailment of wind electricity in china by employing electric
629 boilers for heat and pumped hydro for energy storage, *Applied Energy* 184
630 (2016) 987 – 994.
- 631 [23] M. Andoni, V. Robu, W.-G. Fr  h, D. Flynn, Game-theoretic modeling
632 of curtailment rules and network investments with distributed generation,
633 *Applied Energy* 201 (2017) 174 – 187.
- 634 [24] K. X. Le, M. J. Huang, C. Wilson, N. N. Shah, N. J. Hewitt, Tariff-based
635 load shifting for domestic cascade heat pump with enhanced system energy
636 efficiency and reduced wind power curtailment, *Applied Energy* 257 (2020)
637 113976.
- 638 [25] A. D. Mills, R. H. Wiser, Strategies to mitigate declines in the economic
639 value of wind and solar at high penetration in california, *Applied Energy*
640 147 (2015) 269 – 278.

- 641 [26] Q. Hou, N. Zhang, E. Du, M. Miao, F. Peng, C. Kang, Probabilistic duck
642 curve in high pv penetration power system: Concept, modeling, and em-
643 pirical analysis in china, *Applied Energy* 242 (2019) 205 – 215.
- 644 [27] S. D. Garvey, The dynamics of integrated compressed air renew-
645 able energy systems, *Renewable Energy* 39 (1) (2012) 271–292.
646 doi:<https://doi.org/10.1016/j.renene.2011.08.019>.
647 URL [https://www.sciencedirect.com/science/article/pii/](https://www.sciencedirect.com/science/article/pii/S0960148111004630)
648 [S0960148111004630](https://www.sciencedirect.com/science/article/pii/S0960148111004630)
- 649 [28] G. N. Prodromidis, F. A. Coutelieris, Simulations of economical and
650 technical feasibility of battery and flywheel hybrid energy storage sys-
651 tems in autonomous projects, *Renewable Energy* 39 (1) (2012) 149–153.
652 doi:<https://doi.org/10.1016/j.renene.2011.07.041>.
653 URL [https://www.sciencedirect.com/science/article/pii/](https://www.sciencedirect.com/science/article/pii/S096014811100437X)
654 [S096014811100437X](https://www.sciencedirect.com/science/article/pii/S096014811100437X)
- 655 [29] B. W. Jones, R. Powell, Evaluation of distributed building ther-
656 mal energy storage in conjunction with wind and solar elec-
657 tric power generation, *Renewable Energy* 74 (2015) 699–707.
658 doi:<https://doi.org/10.1016/j.renene.2014.08.031>.
659 URL [https://www.sciencedirect.com/science/article/pii/](https://www.sciencedirect.com/science/article/pii/S096014811400490X)
660 [S096014811400490X](https://www.sciencedirect.com/science/article/pii/S096014811400490X)
- 661 [30] B. Rezaie, B. V. Reddy, M. A. Rosen, Exergy analysis of thermal energy
662 storage in a district energy application, *Renewable Energy* 74 (2015)
663 848–854. doi:<https://doi.org/10.1016/j.renene.2014.09.014>.
664 URL [https://www.sciencedirect.com/science/article/pii/](https://www.sciencedirect.com/science/article/pii/S0960148114005643)
665 [S0960148114005643](https://www.sciencedirect.com/science/article/pii/S0960148114005643)
- 666 [31] A. A. Shukhobodskiy, G. Colantuono, Red wolf: Combining a battery and
667 thermal energy reservoirs as a hybrid storage system, *Applied Energy* 274
668 (2020). doi:<https://doi.org/10.1016/j.apenergy.2020.115209>.
669 URL www.scopus.com
- 670 [32] The Oxford Institute for Energy Studies, The great Dutch gas transition
671 (2019).
- 672 [33] BEIS, Heat in buildings, department for business energy & industrial strat-
673 egy (2020).
674 URL <https://www.gov.uk/government/groups/heat-in-buildings>
- 675 [34] Interreg NWE., Programme Manual v.10 (2019).
- 676 [35] P. Ortiz, S. Kubler, E. Rondeau, J.-P. Georges, G. Colantuono,
677 A. A. Shukhobodskiy, Greenhouse gas emission reduction system
678 in photovoltaic nanogrid with battery and thermal storage reser-
679 voirs, *Journal of Cleaner Production* (2021) 127347doi:<https://doi.org/10.1016/j.jclepro.2021.127347>.
680 [//doi.org/10.1016/j.jclepro.2021.127347](https://doi.org/10.1016/j.jclepro.2021.127347).

681 URL [https://www.sciencedirect.com/science/article/pii/](https://www.sciencedirect.com/science/article/pii/S0959652621015663)
682 [S0959652621015663](https://www.sciencedirect.com/science/article/pii/S0959652621015663)

683 [36] Oxford PV array, [https://shkspr.mobi/blog/2014/12/a-year-of-solar-](https://shkspr.mobi/blog/2014/12/a-year-of-solar-panels-open-data/)
684 [panels-open-data/](https://shkspr.mobi/blog/2014/12/a-year-of-solar-panels-open-data/) (2016).

685 [37] M. Lichman, UCI machine learning repository, [http://archive.ics.uci.](http://archive.ics.uci.edu/ml)
686 [edu/ml](http://archive.ics.uci.edu/ml) (2013).

687 [38] G. Colantuono, A.-L. Kor, C. Pattinson, C. Gorse, PV with multiple storage
688 as function of geolocation, *Solar Energy* 165 (2018) 217–232. doi:10.1016/
689 [j.solener.2018.03.020](https://doi.org/10.1016/j.solener.2018.03.020).

690 [39] Enerdata, Enerdata intelligence + Consulting, [https://www.](https://www.odyssee-mure.eu/publications/efficiency-by-sector/households/electricity-consumption-dwelling.html)
691 [odyssee-mure.eu/publications/efficiency-by-sector](https://www.odyssee-mure.eu/publications/efficiency-by-sector/households/electricity-consumption-dwelling.html)
692 [/households/electricity-consumption-dwelling.html](https://www.odyssee-mure.eu/publications/efficiency-by-sector/households/electricity-consumption-dwelling.html) (2019).

693 [40] ovo energy, How much energy do you use to heat your home? (2010).
694 URL [https://www.ovoenergy.com/guides/energy-guides/](https://www.ovoenergy.com/guides/energy-guides/how-much-heating-energy-do-you-use.html)
695 [how-much-heating-energy-do-you-use.html](https://www.ovoenergy.com/guides/energy-guides/how-much-heating-energy-do-you-use.html)

696 [41] E. E. Agency, Energy consumption by end use per dwelling (2009).
697 URL [https://www.eea.europa.eu/data-and-maps/figures/](https://www.eea.europa.eu/data-and-maps/figures/households-energy-consumption-by-end-uses-5)
698 [households-energy-consumption-by-end-uses-5](https://www.eea.europa.eu/data-and-maps/figures/households-energy-consumption-by-end-uses-5)

699 [42] Ofgem, Ofgem.
700 URL <https://www.ofgem.gov.uk>

701 [43] RTE, Co2 emissions per kwh of electricity generated in france (2019).
702 URL <https://www.rte-france.com/en/eco2mix/co2-emissions>

703 [44] G. Hartley, Northern ireland: reducing dependency on oil-fired heating
704 (2019).
705 URL [https://energysavingtrust.org.uk/blog/](https://energysavingtrust.org.uk/blog/northern-ireland-reducing-dependency-oil-fired-heating)
706 [northern-ireland-reducing-dependency-oil-fired-heating](https://energysavingtrust.org.uk/blog/northern-ireland-reducing-dependency-oil-fired-heating)